



Brussels, 19th of December, 2009

Attention of:
DG TREN - Mr Ismo Gronroos-Saikkala,
Armines - Mr Riviere
VHK - Mr Kemna

CC:
DG TREN – Mr Brisaer
DG ENTR – Ms Lichtenvort

TOPIC: PROPOSAL ON PARTLOAD WEIGHTING AND SEASONAL PERFORMANCE FACTORS

Dear Sirs

Based upon the recent position papers issued, and based on the latest meeting we had on 28/11/2008, we present you with

1. a proposal for part load calculation.
2. a proposal of calculating separate seasonal performance factors for cooling and heating.

The first proposal has been made, to tackle the concern of the heavy weighting factor for part load calculation on heating at -7°C .

The outcome of our investigation is similar to the conclusions made at the Eurovent meeting where the suggestion has been made to use the Strasbourg climate data, as presented by Armines on 25th of November.

The second proposal has been elaborated to give a solution to the problems we have raised in former positions, such as the fact that cooling only products have lower minimum efficiency requirements than reversible products, and the relation that needs to be investigated with lot 1.

We trust that the information contained in this position paper will be of relevance and interest to you. Should you have any questions or require any additional input, please do not hesitate to contact me.

Yours sincerely,

Lars Brückner
Chairman Environment Committee
Japan Business Council in Europe (JBCE)

The Japan Business Council in Europe (JBCE) is an European representative organisation for companies of Japanese parentage that operate in the European Union. A large part of the JBCE membership consists of manufacturers of electrical and electronic equipment, including major producers of leading technology air-conditioning, ventilation and heating products.

JBCE
Rue Montoyer 40, B-1000 Brussels, Belgium
Tel : 32-(0)2-286-5330 / Fax: 32-(0)2-230-5485
E-Mail : info@jbce.org
www.jbce.org

Friedrich P Busch
Director General - EPEE

The European Partnership for Energy and the Environment (www.epeeglobal.org) was formed in September 2000 to represent the interests of the air-conditioning, heat pump and refrigeration industry. Our central mission is to contribute to the development of effective European policies which have the aim to reduce greenhouse gas emissions from the use of refrigerants.

EPEE
14A, rue du Luxembourg, 1000 Brussels, Belgium
Tel : +32-2 732 70 40 / Fax : +32-2 732 71 76
E-Mail : Secretariat@epeeglobal.org /
www.epeeglobal.org

THE REPORT FOR WEIGHTING PROPOSAL

1. Background

We review the weighting values for SCOP and SEER calculation proposed by Armines in task 8 & task 4 final draft and found it quite questionable. Reasons are as follows.

- 1) Weighting of -7 °C is too high compared to the value experiences tell.
- 2) Weighting shape is unusual. It should be high in the middle range. Otherwise uncalculated part appears too large.
- 3) Sales value of countries such as Romania, Bulgaria and Baltic three countries appears too high based on their GDP per capita and summer temperature.
- 4) Operation hours are too short that exaggerates the thermo-off time and crankcase heater operation hours.
- 5) R factor used in calculation for supplemental heater effect is confusing.

As such, we have decided to provide a new proposal, which takes into account the issues that have been raised in previous comments during stakeholder consultations and other meetings.

2. Assumption

We calculate the weighting under following assumptions.

- 1) Building load for heating is assumed to be linear having 100% load at 2 °C and 0% at 15.5 °C. This value is decided from the data of the EuP lot 10 task 4 report annex B Figure 1; Heating and cooling EU average load curves. Only linear part is considered. Cooling load is 100% at 35°C and 0% at 13°C. Other building load considering sizing effect may be evaluated.

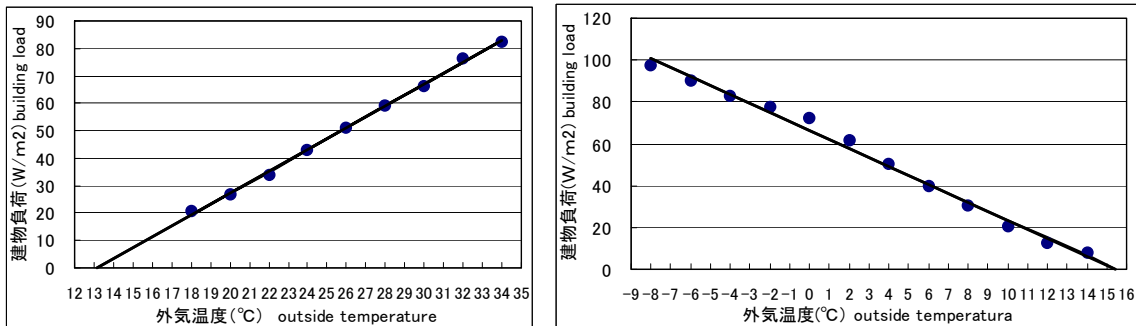


Figure 1 Cooling and Heating load

Load values are decided as follows;

Table 1. Cooling load

Ambient Outdoor (°C)	Cooling load (W/m ²)	Load Ratio	Rounded Load (%)
0	27.15	0.31	30
25	47.01	0.54	55
30	66.88	0.77	75
35	86.74	1.00	100

Table 2. Heating load

Ambient Outdoor (°C)	Heating load (W/m ²)	Load Ratio	Rounded Load (%)
15.5	0	0.00	0
2	100	1.00	100

	Ambient Outdoor (°C)	Heating load (W/m ²)	Load Ratio	Rounded Load (%)
Proposal on partload weighting and seasonal performance factors			1.67	165
Proposal 1: proposal for part load calculation		57.9	1.00	100
	7	36.4	0.63	60
	12	14.9	0.26	25

Not only heating but also cooling is to be calculated with the same method.

- 2) Sales volumes of some countries in the EUP – lot 10 report appear excessively high compared to their GDP per capita. Therefore we estimate sales volumes of respective countries based on the JRAIA (Japan Refrigeration and Air conditioning Industry Association) 2007 sales data estimation. For data that is not available, simplified corrections have been done. For example, for Slovakia and Slovenia the values indicated in the task report are discounted to 1/3.
- 3) Weighting of each calculating bin is separated evenly between measuring points by temperature and not by energy (the US IPLV method). Performances is assumed to be the same in each bin.
- 4) The definition of season in the task report is used. Cooling season May 1st to 30th September. Heating season October to April. If there is no load in heating season, it is regarded as thermo-off time. If there is no load in cooling season, it is considered as stand-by.
- 5) Supplemental heater is directly involved to the performance at -7 °C. R factor is not used.
- 6) Hourly temperature data of cities are taken from US DOE EnergyPlus web. Capital cities are chosen in first priority. If only a city data other than capital is available, it is used instead of capital. Spain and Italy are divided into two regions and calculated with the same method of the task report.

http://apps1.eere.energy.gov/buildings/energyplus/cfm/weather_data2.cfm/region=6_europe_wmo_region_6

For some countries without available data, we calculate as follows; Sales weight of Malta is added to Cyprus. Baltic three countries are represented by Lithuania. The weight of Bulgaria is added to Romania.

Table 2. Weighting of each country

	JRAIA Estimation Weight (%)	Task report Weight (%)
Austria	0.30	0.22
Belgium	2.04	1.52
Bulgaria	2.51	3.62
Cyprus	0.92	0.54
Czech	0.53	0.40
Denmark	1.05	0.78
Estonia	0.27	0.20
Finland	0.53	0.39
France	9.46	8.89
Germany	2.55	2.49
Greek	9.89	7.42
Hungary	1.40	1.25
Ireland	0.42	0.31
Italy	29.29	25.34
Latvia	0.45	0.33
Lithuania	0.66	0.49
Luxembourg	0.10	0.07
Malta	0.25	0.19
Netherlands	1.09	2.37
Poland	0.65	0.48
Portugal	3.11	1.17
Romania	2.25	10.17
Slovakia	1.14	2.54
Slovenia	0.42	0.94
Spain	23.01	21.15

Proposal on partload weighting and seasonal performance factors
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Sweden	1.57	0.67
UK	4.16	6.02
Total	100	100

Proposal on partload weighting and seasonal performance factors
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Table 4. Weighting coefficient for cooling.

TEMP	Load	Hour	Load*Hr	Load*Hr Sub total	Weighting Coefficient	Rounded Coefficient
13	0%	95	0.0			
14	5%	159	7.2			
15	9%	176	16.0			
16	14%	179	24.4			
17	18%	202	36.6			
18	23%	214	48.7			
19	27%	221	60.2			
20	32%	220	70.0	426.0	0.330	33%
21	36%	209	75.9			
22	41%	212	86.9			
23	45%	218	98.9			
24	50%	198	98.9			
25	55%	181	98.9	480.9	0.372	37%
26	59%	165	97.3			
27	64%	136	86.8			
28	68%	119	80.9			
29	73%	92	67.2			
30	77%	72	55.8	276.6	0.214	21%
31	82%	47	38.6			
32	86%	39	34.1			
33	91%	29	26.7			
34	95%	22	21.0			
35	100%	19	19.2	108.8	0.084	9%
36	105%	14	14.7			
37	109%	10	10.4			
38	114%	7	7.8			
39	118%	4	4.7			
40	123%	2	3.0			
41	127%	0	0.4			
42	132%	1	0.8			
43	136%	0	0.2			
Total		3,263	1,292.3	1,292.3	1.000	100%

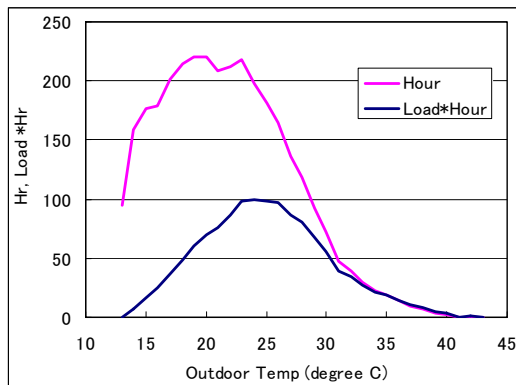


Figure 2. Cooling Hour and Hour x load distribution

Proposal on partload weighting and seasonal performance factors
 Proposal 1: proposal for part load calculation

Table 6. Weighting coefficients for heating.

TEMP	Load	Hour	Load*Hr	Load*Hr Sub total	Weighting Coefficients	Rounded Weighting Coefficients
-22	278%	0.0	0.0			
-21	270%	0.1	0.2			
-20	263%	0.3	0.7			
-19	256%	0.5	1.2			
-18	248%	0.3	0.9			
-17	241%	0.6	1.5			
-16	233%	0.7	1.7			
-15	226%	0.9	2.1			
-14	219%	1.3	2.8			
-13	211%	1.9	3.9			
-12	204%	2.2	4.5			
-11	196%	3.2	6.2			
-10	189%	5.6	10.6			
-9	181%	7.9	14.3			
-8	174%	13.0	22.6			
-7	167%	18.9	31.6	315.2	0.118	12%
-6	159%	21.8	34.7			
-5	152%	25.7	39.0			
-4	144%	37.3	53.9			
-3	137%	60.6	83.0			
-2	130%	82.7	107.2			
-1	122%	107.7	131.6			
0	115%	140.7	161.6			
1	107%	171.6	184.3			
2	100%	170.5	170.5	1,127.3	0.420	42%
3	93%	190.5	176.4			
4	85%	229.9	195.8			
5	78%	252.9	196.7			
6	70%	256.6	180.6			
7	63%	263.0	165.6	851.0	0.317	32%
8	56%	296.6	164.8			
9	48%	297.8	143.4			
10	41%	302.9	123.4			
11	33%	297.9	99.3			
12	26%	306.9	79.6	388.1	0.145	14%
13	19%	273.8	50.7			
14	11%	244.9	27.2			
15	4%	214.8	8.0			
Total		4,304	2,681.8	2,681.8	1.000	100%

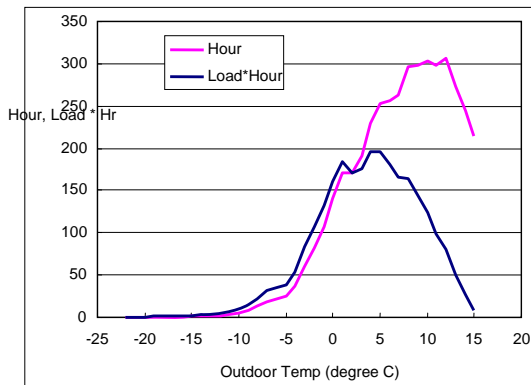


Figure 3. Heating hours and Load*Hr

Proposal on partload weighting and seasonal performance factors
 Proposal 1: proposal for part load calculation

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5. Operating Hours

These calculations lead to the following operation and non-operation hours.

Table 7. Cycle operation hours

	Air conditioners		Reversible heat pump		Heating only	
	NON-INV	INV	NON-INV	INV	NON-INV	INV
Cooling, H_C	1149	2434	1149	2434	0	0
Heating, H_H	0	0	2187	3468	2187	3468
Off mode, H_{OFF}	5,088		0		3,672	
Standby, H_{SB}	409			0		
Heating Thermo-off, H_{HTO}	0	0	2901	1620	2901	1620
Cooling Thermo-off, H_{CTO}	2114	829	2114	829		
Total	8,760	8760	8,760	8760	8,760	8760

Table 8. Crank case heater operation

		Crankcase, H_{CK}		
		Air conditioners	Reversible heat pump	Heating only
control	Non-Inv	2513	5424	2901
	Inv	1238	2858	1620
no control	Non-Inv	3,672	8,760	5,088
	Inv			

Note; no control; CH is always connected to power line.

control; CH is controlled by main thermo. (B contact of compressor relay)

smart control is evaluated by 8 hours test. Average power of 8 hours after stop is used for the calculation.

6. Conclusion

1) Cooling

Seasonal Efficiency should be calculated according to following formula and coefficients.

$$SEER_{on} = \frac{1}{\frac{A}{EER_A} + \frac{B}{EER_B} + \frac{C}{EER_C} + \frac{D}{EER_D}}$$

Testing Point	Measuring	Part Load Ratio (%)	Indoor Temperature		Outdoor Temperature Dry bulb(°C)	Weighting Coefficients (%)
			Dry bulb(°C)	Wet bulb(°C)		
A	EER _A , P _{CA}	100	27	19	35	9
B	EER _B , P _{CB}	75			30	21
C	EER _C , P _{CC}	55			25	37
D	EER _D , P _{CD}	30			20	33

2) Heating

$$SCOP_{on} = \frac{1}{\frac{A}{COP_A} + \frac{B}{COP_B} + \frac{C}{COP_C} + \frac{D}{COP_D}}$$

Testing Point	Measuring	Part Load Ratio (%)	Indoor Temperature Dry bulb(°C)	Outdoor Temperature		Weighting Coefficients (%)
				Dry bulb(°C)	Wet bulb(°C)	
A	COP _A , P _{HA}	100	20	2	1	42
B	COP _B , P _{HB}	60		7	6	32
C	COP _C , P _{HC}	165*		-7	-8	12
D	COP _D , P _{HD}	25		12	11	14

*If heat pump capacity at -7°C outdoor is less than 165% of the capacity at 2°C outdoor, that part of heating capacity is covered by resistive heating. This results in COP of 1 in no operation case. If operating range is limited at -7 °C, whole load below -7°C would be covered by resistive heater. In such case, this calculation results in 1-2% overestimate SCOP value.

SCOP_C may be calculated from separate measurement of heatpump only operation and resistive heater effect as follows.

$$R = 1 - \frac{P_{HC-HP}}{1.65 \cdot P_{HA}}$$

$$COP_C = \frac{1}{\frac{1-R}{COP_{C-HP}} + R}$$

R; Supplement heater ratio at -7°C

P_{HC-HP}; Capacity measured with only heatpump operation

COP_{C-HP}; COP measured with only heatpump operation

PROPOSAL2: PROPOSAL FOR SEPARATE SEASONAL PERFORMANCE FACTORS FOR COOLING & HEATING.

In reviewing the task 8 report, EPEE & JBCE have raised several issues. We believe that some of the problems can be solved by separating the cooling function and heating function for both the rating (labeling) and definition of minimum efficiency requirements. Instead of having separate minimum requirements for cooling only, heating only and reversible airconditioners. We feel that the latter approach is technology based, and it is best to define for these technologies the same efficiency requirements on their specific function for cooling and heating.

Therefore, instead of working with an APF factor, we propose to split up the efficiency factor into a seasonal performance factor for cooling (SPF_c) and a seasonal performance factor for heating (SPF_h), bearing in mind that both these factors need to incorporate the standby and off mode losses.

We believe that the following facts support our proposal and would make it easier for the commission to define the minimum efficiency requirements. It would also help customers to make selections based on the best possible information available to them.

1. APF is confusing and unclear for end users:

The APF value is a very theoretical value, that gives the weighted average efficiency in cooling and heating of a reversible airconditioner. However, it does not show the actual efficiency of the product either in cooling and in heating, since it is only a weighted average of cooling and heating. It is suitable to compare reversible heatpumps in average European weather condition. However, end users cannot compare APF with SEER and SCOP. even if the task 8 report of Lot 10 proposes to indicate all APF, SEER and SCOP values in the label.

The problem is that the APF value is always lower than the SEER value, since it is a weighted averaging of cooling and heating. endusers will be pushed to select cooling-only products, since the SEER value is higher than the APF value, although reversible heatpumps have higher SEER value. In the end they would buy products with lower efficiency. Moreover, they would not recognise the benefit of heat pump in heating.

2. Possible adjustment for cooling-only and reversible products on SPF_c

Introducing a separate cooling factor and heating factor enables us to obtain separate minimum efficiency requirements which will reflect actual efficiency either in heating or cooling. It will solve the present problem that the minimum requirement for cooling-only products are less stringent than for reversible products.

3. Possible adjustment for heating-only and reversible products on SPF_h

Having a separate heating performance enables us to compare the heating efficiencies of products in lot 10, with the efficiency of products in scope of lot 1. It should be noted that it also reflects contributions of heat pumps to providing certain amount of renewable energy.

In view of the upcoming directive on renewable energy sources, the indication of SPF will be most important.

4. Balancing heating and cooling performance

One thing that needs to be considered is to provide some allowance in the minimum efficiency criteria for cooling and heating in case of reversible heatpumps having excellent performance in one function (cooling/heating). Using the APF value allows a designer to have a certain freedom in order to choose where he selects the energy efficient solutions in cooling and heating.

This is in line with the customer selections, that will choose the product best performing in heating or in cooling based on their personal needs and climate zone.

EUP requirements are based on average European climate. As such, some allowance is required to optimise the products towards warmer or colder climate. In view of the EUP – methodology, this means that the unit, designed to perform very well in cooling, should get some allowance for performance in heating and vice versa.

Conclusion

The minimum efficiency requirements of task 8 need to be reviewed in line with this proposal. The energy label should be reviewed accordingly.

In practice, two energy labels should be attached to those products which have both cooling function and heating function.

➤taking into account proposal 1, we propose the following calculation method for SPF_c and SPF_h

NOTE: For the purpose of this paper, we use the terms SPF_c and SPF_h instead of SEER and SCOP used in the task 8 and task 4 report. In view of RES, it is necessary to redefine the terms.

General operation hours for cooling and heating

	Air conditioners		Reversible heat pump		Heating only	
	NON-INV	INV	NON-INV	INV	NON-INV	INV
Effective Cooling, H _{CE}	1149	2434	1149	2434	0	0
Effective Heating, H _{HE}	0	0	2187	3468	2187	3468
Off mode, H _{OFF}	5,088		0		3,672	
Cooling Standby, H _{SBC}	409					
Heating Standby, H _{SBH}	0					
Heating Thermo-off, H _{HTO}	0	0	2901	1620	2901	1620
Cooling Thermo-off, H _{CTO}	2114	829	2114	829		
Total	8,760	8760	8,760	8760	8,760	8760
Equivalent Hours cooling H _C *	1292					
Equivalent Hours heating H _H *	2682					

* based on 100% part load ratio equivalent hours.

		Crankcase, H _{CK}		
		Air Conditioners	Reversible Heat pump	Heating only
control	Non-Inv	2513	5424	2901
	Inv	1238	2858	1620
no control	Non-Inv	3,672	8,760	5,088
	Inv			

Calculation of SPF_c

1. determine SEER_{on} of the appliance:

Testing Point	Measuring	Part Load Ratio (%)	Indoor Temperature		Outdoor Temperature Dry bulb(°C)	Weighting Coefficients (%)
			Dry bulb(°C)	Wet bulb(°C)		
A	EERA, PCA	100	27	19	35	9
B	EERB, PCB	75			30	21
C	EERC, PCC	55			25	37
D	EERD, PCD	30			20	33

$$SEER_{on} = \frac{1}{\frac{A}{EER_A} + \frac{B}{EER_B} + \frac{C}{EER_C} + \frac{D}{EER_D}}$$

2. Calculation of SPF_c

$$SPF_c = \frac{H_C \times P_{CA}}{\frac{H_C \times P_{CA}}{SEER_{on}} + H_{CTO} \times P_{CTO} + H_{SBC} \times P_{SBC} + H_{OFF} \times P_{OFF} + H_{CK} \times P_{CK}}$$

Calculation of SPF_h

1. determine the $SCOP_{on}$ of the appliance:

Testing Point	Measuring	Part Load Ratio (%)	Indoor Temperature Dry bulb(°C)	Outdoor Temperature		Weighting Coefficients (%)
				Dry bulb(°C)	Wet bulb(°C)	
A	COPA, PHA	100	20	2	1	42
B	COPB, PHB	60		7	6	32
C	COPC, PHC	165*		-7	-8	12
D	COPD, PHD	25		12	11	14

$SCOP_C$ may be calculated from separate measurement of heatpump only operation and resistive heater effect as follows.

$$R = 1 - \frac{P_{HC-HP}}{1.65 \cdot P_{HA}}$$

$$COP_C = \frac{1}{\frac{1-R}{COP_{C-HP}} + R}$$

R; Supplement heater ratio at -7°C

P_{HC-HP} ; Capacity measured with only heatpump operation

COP_{C-HP} ; COP measured with only heatpump operation

$$SCOP_{on} = \frac{1}{\frac{A}{COP_A} + \frac{B}{COP_B} + \frac{C}{COP_C} + \frac{D}{COP_D}}$$

2. Calculation of SPF_h

$$SPF_h = \frac{H_H \times P_{HA}}{\frac{H_H \times P_{HA}}{SCOP_{on}} + H_{HTO} \times P_{HTO} + H_{SBH} \times P_{SBH} + H_{OFF} \times P_{OFF} + H_{CK} \times P_{CK}}$$

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